# JOHN DAY 

TRANSPORTATION STUDY

JULY 2021

PREPARED FOR:

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## SECTION 1. INTRODUCTION

The purpose of this transportation impact analysis is to identify potential transportation system needs triggered by the proposed Ironwood Estates (Phase 2 and 3) and The Ridge (Phase 1 and 2) developments located in John Day, OR.

Included in the following sections is a documentation of existing transportation conditions, a summary of the assumptions and methodologies used to analyze future transportation conditions, a detail of traffic operating conditions and a summary of recommendations related to the proposed project.

## PROJECT AREA

The proposed Ironwood Estates (Phase 2 and 3) development will be located off Valley View Drive and Government Entry Road, at the north end of the City. The proposed Ridge (Phase 1 and 2) development will be located at the east end of the City, to the south of US 26. The following intersections were evaluated as study intersections, with their intersection control listed:

- W. Main Street (US 26) / Patterson Bridge Road (existing stop controlled on the side street)
- W. Main Street (US 26) / NW 3rd Avenue (existing stop controlled on the side street)
- E. Main Street (US 26) / NW 3 ${ }^{\text {rd }}$ Avenue (existing stop controlled on the side street)
- E. Main Street (US 26) / The Ridge Access (proposed stop controlled on the side street)


## SECTION 2. EXISTING CONDITIONS

Much of the land within the study area is rural, except for land surrounding W Main Street through downtown John Day. As a result, many roadways are not constructed to urban standards. Evaluating the transportation impacts of the proposed hotel and conference center development requires an understanding of the current transportation facilities in this area. This section includes descriptions of existing infrastructure to serve pedestrian, bicycle, transit and motor vehicle modes of travel in the immediate study area.

## PEDESTRIAN AND BICYCLE SYSTEM

An inventory of existing pedestrian and bicycle facilities was conducted to summarize current pedestrian and bike facilities within the project area. Table 1 shows the key roadways, along with existing pedestrian and bicycle facilities. Due to the rural nature of the abutting land uses, many streets in the study area have not been improved to urban standards and generally lack accommodation for pedestrian and bicycle users.

W Main Street is an important connection for pedestrian and bicycle travel in the City. It provides the only current direct route for pedestrians and bicyclists to access all parts of the City. Those walking or biking along this highway often must walk along the shoulder or share the travel lane with motor vehicles. In addition, frequent driveways negatively impact the walking experience and introduce conflict points between pedestrians and motor vehicles. Motor vehicle traffic volumes along this segment of the highway is over 5,000 vehicles per day and the posted speed is 35 miles per hour. These conditions are generally not conducive to comfortable shared walking and biking travel conditions. W Main Street through John Day is also designated as part of the Old West Oregon Scenic Bikeway. Much of this route lacks accommodations for bicyclists.

Pedestrian and bicycle count data during the evening peak period was collected at the study intersections ${ }^{1}$. The count data shows that the only pedestrian activity observed occurred at the W Main Street / NW 3rd Avenue intersection (8 crossings during the p.m. peak period). No bicycle activity was recorded at the study intersections during the p.m. peak period.

[^0]TABLE 1: STUDY AREA PEDESTRIAN AND BICYCLE CHARACTERISTICS

| ROADWAY (LIMITS) | PEDESTRIAN FACILITIES | BIKE FACILITIES |
| :--- | :---: | :---: |
| W MAIN STREET - US 26 / US 395 <br> (PATTERSON BRIDGE ROAD TO 3RD <br> AVENUE) | Sidewalk on north side from 3rd <br> Avenue to the west for 0.25 <br> miles; Intermittent sidewalks on <br> south side | None |

## TRANSIT SYSTEM

Transit service is provided in John Day and other nearby cities by the Grant County People Mover via several fixed bus routes, a Dial-a-Ride service and two deviated fixed route systems. The People Mover connects riders in John Day to nearby cities including Bend, Redmond, Prineville, Mount Vernon, Monument, Pendleton, Walla Walla, Burns, Prairie City and Baker City. The Bend, Redmond, Prineville, Mount Vernon route runs Monday, Wednesday, and Friday; the Monument route runs on Thursdays; the Pendleton and Walla Walla route runs on Tuesdays; the Burns route runs on the 1st, 3rd, and 5th Thursday of the month; and the Prairie City and Baker City route runs on the 2nd and 4th Thursday of the month. Each of these routes typically depart John Day in the morning and return in the evening.

The deviated fixed route services in the John Day valley run Monday through Friday. The route will deviate $1 / 2$ mile from the fixed route line. The PC MV Route runs between Prairie City and Mt Vernon three times a day, at $7 \mathrm{am}, 12 \mathrm{pm}$ and 6 pm . The JD CC Loop runs a set route in John Day and Canyon City every hour, beginning at 7 am and ending at 6 pm . Both the PC MV Route and the JD CC Loop are free.

The Dial-a-Ride, or Demand Response service runs Monday through Friday 8 am to 6 pm and Saturday 9 am to 4 pm . This service picks and drops off passengers at a location of their choosing. Anyone is eligible to ride this service, and it is available in John Day, Canyon City, Mt Vernon and Prairie City.

The deviated fixed routes have transit stops throughout John Day, with 56 stops in and around the City. Most of the intercity routes pick-up and drop-off passengers at the People Mover Bus Depot
located on NE Dayton Street near at NE 1st Avenue. However, the Monument to John Day route pick-ups and drop-offs passengers at the Senior Center parking lot on NE Dayton Street south of NE 1st Avenue.

Transit users in the study area are generally less than one quarter mile from the closest bus stop (within the typical trip length for the average walking trip).

## ROADWAY SYSTEM

The major characteristics of the roadways in the study area are summarized in Table 2. W Main Street provides higher capacity motor vehicle movement through the study area. It is classified by the state as a Statewide Highway and runs east-to-west maintaining a two-lane (i.e., one through lane in each direction) to three-lane cross-section (i.e., one through lane in each direction and a center turn lane) through the study area. Posted speeds along the highway in the study area range between 25 and 35 miles per hour. It is designated as a scenic byway and freight route, and the segment near the NW 3rd Avenue intersection is within an urban business area.

Patterson Bridge Road and Bridge Street run north-to-south from W Main Street, providing the only current crossings of the John Day River. 3rd Avenue runs east-to-west through the center of John Day, connecting to W Main Street. These streets are classified as collectors and generally have lower vehicle-carrying capacity than the highway. All other roadways in the study area are local streets and primarily serve local traffic traveling to and from the highway.

TABLE 2: STUDY AREA ROADWAY CHARACTERISTICS

| ROADWAY (LIMITS) | FUNCTIONAL <br> CLASSIFICATION* | CROSS SECTION | SPECIAL <br> DESIGNATIONS |
| :--- | :---: | :---: | :---: |
| W MAIN STREET - US $26 /$ US 395 <br> (PATTERSON BRIDGE ROAD TO 3RD <br> AVENUE) | Statewide | 2 to 3 lanes | Scenic Byway; <br> Freight Route; Urban <br> Business Area (City <br> limits to 3rd Avenue) |
| PATTERSON BRIDGE ROAD <br> (US 26 / US 395 TO NORTHERN <br> TERMINUS) | Collector | 2 lanes | None |

*Source: Oregon Highway Plan; John Day Transportation System Plan, December 1996.

To determine intersection operations, turning movement counts were conducted at study intersections during the weekday evening peak period (4 to 6 p.m.). The raw traffic count data is included in the Appendix.

## DAILY MOTOR VEHICLE VOLUMES

Daily motor vehicle count data was also collected at the two existing motor vehicle crossings of the John Day River, including along NW Bridge Street near the NW 7th Avenue intersection and Patterson Bridge Road north of US 26. The count data indicates that approximately 1,266 vehicles use NW Bridge Street, and 898 vehicles use Patterson Bridge Road to cross the John Day River during an average weekday. The highest number of vehicle crossings occurred during the p.m. peak hour at both locations (4:00 p.m.), with 123 crossings at NW Bridge Street and 100 at Patterson Bridge Road.

## INTERSECTIION OPERATIONS

This section discusses the existing conditions for motor vehicles at the study intersections, including an analysis of traffic operations.

## Intersection Performance Measures

Level of service (LOS) ratings and volume-to-capacity (v/c) ratios are two commonly used performance measures that provide a good picture of intersection operations. Agencies often incorporate these performance measures into their mobility standards. Descriptions are given below:

- Level of service (LOS): A "report card" rating (A through F) based on the average delay experienced by vehicles at the intersection. LOS $A, B$, and $C$ indicate conditions where traffic moves without significant delays over periods of peak hours travel demand. LOS D and E are progressively worse operation conditions. LOS F represents conditions where average vehicle delay has become excessive, and demand has exceeded capacity.
- Volume-to-capacity (v/c) ratio: A decimal representation (typically between 0.00 and 1.00 ) of the proportion of capacity that is being used at a turn movement, approach leg, or intersection. It is determined by dividing the peak hour traffic volume by the hourly capacity of a given intersection or movement. A lower ratio indicates smooth operations and minimal delays. As the ratio approaches 1.00, congestion increases, and performance is reduced. If the ratio is greater than 1.00, the turn movement, approach leg, or intersection is oversaturated and usually results in excessive queues and long delays.


## Jurisdictional Mobility Standards

The mobility standards for the study intersections vary according to the agency of jurisdiction for each roadway. All of the study intersections are under ODOT jurisdiction. ODOT requires a volume
to capacity ratio of 0.85 or less to be maintained for highway movements and a volume to capacity ratio of 0.95 or less to be maintained for the minor approaches ${ }^{2}$.

## Existing Operating Conditions

Motor vehicle conditions were evaluated during the p.m. peak hour at the study intersections (see Table 3). During the peak hour, all study intersections operate well within the adopted mobility standards.

TABLE 3: EXISTING STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY STANDARD | DELAY | LOS | V/C |
| :---: | :---: | :---: | :---: | :---: |
| W. MAIN STREET / PATTERSON BRIDGE ROAD | W. Main Street: $0.85 \text { V/C; }$ <br> Minor: <br> Approaches: 0.95 V/C | 13 | A/B | 0.18 |
| W. MAIN STREET / NW 3RD AVENUE |  | 11 | A/B | 0.10 |
| E. MAIN STREET / NE 3RD AVENUE |  | 11 | A/B | 0.19 |
| E. MAIN STREET / THE RIDGE ACCESS |  | - | - | - |

$\mathrm{v} / \mathrm{c}=$ Volume-to-Capacity Ratio of Worst Movement
Delay = Average Intersection Delay (sec.) of Worst Approach
LOS = Level of Service of Major Street/Minor Street

## SAFETY ANALYSIS

Five years of available collision data (2014-2018) for the study intersections was obtained from Oregon Department of Transportation (ODOT) and used to evaluate the collision history ${ }^{3}$. Three crashes were recorded, two at the W. Main Street / Patterson Bridge Road intersection and one at the E. Main Street / NE $3^{\text {rd }}$ Avenue intersection, over the five-year period.

Crash rates at study intersections were calculated to identify problem areas in need of mitigation. The total number of crashes experienced at an intersection is typically proportional to the number of vehicles entering it, therefore, a crash rate describing the frequency of crashes per million entering vehicles (MEV) is used to determine if the number of crashes should be considered high. Using this technique, a collision rate of 1.0 MEV or greater is commonly used to identify when collision occurrences are higher than average and should be further evaluated. As shown in Table 4, crash rates calculated at all study intersections are well below this threshold, indicating the frequency of collisions is typical for the volume of traffic served.

[^1]TABLE 4: CRASH DATA SUMMARY (2014-2018)

| INTERSECTION | TOTAL CRASHES | CRASH TYPE |  | CRASH SEVERITY |  | $\begin{aligned} & \text { COLLISION } \\ & \text { RATE } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | REAR END | TURN | PDO* | POSSIBLE INJURY |  |
| W. MAIN STREET / PATTERSON BRIDGE ROAD | 2 | 1 | 1 | 0 | 2 | 0.28 |
| W. MAIN STREET / NW 3RD AVENUE | 0 | 0 | 0 | 0 | 0 | 0.00 |
| E. MAIN STREET / NE 3RD AVENUE | 1 | 1 | 0 | 1 | 0 | 0.21 |

[^2]
## SECTION 3: ASSUMPTIONS AND METHODOLOGIES

This section outlines key assumptions and methodologies that were used to analyze future conditions and identify any potential impacts at study intersections. Areas of interest covered in this section are trip generation, trip distribution and background traffic growth.

## PROJECT DESCRIPTION

The proposed Ironwood Estates Phase 2 development will consist of 17 single family units (see Figure 1), while the proposed Ironwood Estates Phase 3 will consist of 56 duplex units along with a 2,500 square foot common building (see Figure 1).

FIGURE 1: IRONWOOD ESTATES PHASES 2 AND 3 SITE PLAN


The proposed Ridge development is proposed to occur is two phases as shown in Figure 2, with a proposed 11 single family units in Phase 1 (parcel 1; lots 1-11). Phase 2 is expected to occur among parcels 2 to 5 , for a total area of about 63 acres. Several assumptions were utilized to determine the amount of buildable land and sizes of potential development to base trip generation estimates (see Table 5). Average assumptions regarding development densities that can reasonably be expected were utilized to estimate the net quantities of potential development. The development assumptions were based on single family units, and a minimum lot size of 10,000 square feet per unit for the Residential General (RG) zone. Overall, an estimated 221 single family units will be assumed for Phase 2. This represents a conservative estimate for the potential development that could occur within the future Phase 2.

TABLE 5: THE RIDGE PHASE 2 DEVELOPMENT ASSUMPTIONS

| ZONING | PARCEL | SIZE | DEVELOPMENT DENSITY | NET SIZE |
| :---: | :---: | :---: | :---: | :---: |
| RG | Parcel 2 | 20.75 acres | 20 percent reduction for infrastructure and unbuildable areas <br> 10,000 square foot minimum lot size per unit* | 72 single family units |
|  | Parcel 3 | 12.24 acres |  | 43 single family units |
|  | Parcel 4 | 19.89 acres |  | 69 single family units |
|  | Parcel 5 | 10.75 acres |  | 37 single family units |
|  | Total | 63.63 acres |  | 221 single family units |

[^3]

## SITE ACCESS

The Ironwood Estates Phase 2 project has two proposed accesses to Valley View Drive. Both proposed accesses result in cul-de-sacs to the west. Both accesses are recommended to be constructed as residential streets ${ }^{4}$. The access spacing standard for a roadway of this type is 300 feet ${ }^{5}$. The proposed access points will meet this standard.

The Ironwood Estates Phase 3 project has one proposed access to Government Entry Road. The access is recommended to be constructed as a residential street. The access spacing standard for a roadway of this type is 300 feet. The proposed access would not meet the City standard of 300 feet minimum spacing between intersections, as Valley View Drive is approximately 150 feet north of the proposed access. Although the proposed driveway would be located 150 feet closer than the 300 -foot spacing standard, no operational or safety issues are anticipated due to the low number of vehicles using the driveway, and a deviation to the Code will be required.

The proposed Ridge development will have one access to E. Main Street. E. Main Street is classified as a statewide highway with a posted speed of 35 mph adjacent to the project site. The access spacing standard for a roadway of this type is 500 feet. The proposed driveway to E. Main Street would be approximately 700 feet east, and 1,150 feet west of the nearest driveways, complying with the spacing standard.

## INTERNAL SITE CIRCULATION

The proposed site plan for Ironwood Estates (shown earlier in Figure 1) shows two connections to Valley View Drive serving Phase 2, and one connection to Government Entry Road serving Phase 3. These roadways will provide access to residential lots. The proposed roadways will provide adequate circulation to the surrounding existing roadway network, and internally within the site.

The proposed site will provide streets with a 25 -foot paved width, allowing for two 10 -foot travel lanes for the circulation of vehicle traffic and a 5 -foot width for pedestrians to walk along the shoulder. Bicyclists will share the roadways with motor vehicles along the internal local streets. The proposed internal pedestrian and bicycle facilities are adequate for the site given the low traffic volumes and speeds expected.

The proposed site plan for The Ridge (shown earlier in Figure 2) shows one connection to E. Main Street serving Phase 1, and one additional connection to SE Hillcrest Road serving the future Phase. These roadways will provide access to residential lots. The proposed roadways will provide adequate circulation to the surrounding existing roadway network, and internally within the site.

The proposed site will provide streets with a 25 -foot paved width, allowing for two 10 -foot travel lanes for the circulation of vehicle traffic and a 5-foot width for pedestrians to walk along the shoulder. Bicyclists will share the roadways with motor vehicles along the internal local streets. The

[^4]proposed internal pedestrian and bicycle facilities are adequate for the site given the low traffic volumes and speeds expected.

## PLANNING HORIZONS

The planning horizon years selected for analysis are 2023 and 2025, which represent the expected year of build-out and occupancy for the proposed projects. Four scenarios were evaluated to allow for the identification of capacity constraints associated with proposed project, including:

- 2023 Background Conditions - Existing traffic volumes plus background traffic growth.
- 2023 Project Conditions - Existing traffic volumes plus background traffic growth, with the added traffic associated with the proposed project (Ironwood Estates Phase 2 and The Ridge Phase 1).
- 2025 Background Conditions - Existing traffic volumes plus background traffic growth.
- 2025 Project Conditions - Existing traffic volumes plus background traffic growth, with the added traffic associated with the proposed project (Ironwood Estates Phase 3 and The Ridge Phase 2).

Two additional sensitivity options were tested for the 2025 Project Conditions Scenario that assumed full build-out of the Innovation Gateway Area site, both without and with associated transportation network improvements. These scenarios include the proposed Ironwood Estates and The Ridge projects, a hotel and conference center, offices, a wastewater treatment plant, parks and open space and a campground north of the John Day River, and parks and open space, public works facility and greenhouses south of the river. The sensitivity scenario with the transportation network improvements also includes the following (see Figure 3):

1) 7th Street extension from Bridge Street to Patterson Bridge Road
2) Government Entry Road construction from Patterson Bridge Road to Valley View Drive
3) Gateway Drive construction from 7th Street to Government Entry Road
4) Improvements along W Main Street from Patterson Bridge Road to Johnson Drive, and Johnson Drive construction north of W Main Street
5) 7th Street east extension, and Holmstrom Road and bridge across the John Day River connecting $7^{\text {th }}$ Street with NE 3rd Street

FIGURE 3: IMPROVEMENTS ASSUMED WITH SENSITIVTY SCENARIO


## BACKGROUND TRAFFIC

In addition to the trips generated from the proposed project, a half percent background traffic growth rate was applied to existing volumes to represent traffic volumes in 2023 and 2025. Although traffic volumes along W. Main Street adjacent to the project site have been steady or even declining slightly in recent years (see Table 6), as a conservative approach the background traffic growth rate would cover any in-process developments that could potentially build-out and increase traffic volumes before the completion of the proposed projects in 2023 and 2025.

TABLE 6: VOLUME DATA ALONG MAIN STREET

| LOCATION | YEAR | AADT* |
| :--- | :---: | :---: |
| MAIN STREET (US 26) | 2011 | 4,500 |
| MILE POINT 161.30 | 2019 | 4,100 |
| ANNUAL GROWTH RATE (2011 TO 2019) | $\mathbf{- 1 . 1 \%}$ |  |
| *Source: ODOT Transportation Volume Tables, 2011 and 2018 |  |  |

Trip generation is the method used to estimate the number of vehicles that are added to the surrounding roadway network as a result of proposed project. The trip generations for the proposed projects were estimated using the Single-Family Detached Housing (ITE Code 210) and Recreational Community Center (ITE Code 495) land uses as reported by the Institute of Transportation Engineers (ITE) ${ }^{5}$.

Table 7 summarizes the expected trip generation for each phase of each proposed project. As shown, the proposed sites are expected to generate approximately 307 (192 in, 115 out) p.m. peak hour trips.

[^5]TABLE 7: TRIP GENERATION FOR THE PROPOSED PROJECTS

| LAND USE | TRIP GENERATION SOURCE | LAND USE SIZE | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | IN | OUT | TOTAL |
| IRONWOOD ESTATES PHASE 2 |  |  |  |  |  |
| SINGLE-FAMILY <br> DETACHED HOUSING | ITE Code 210 | 17 units | 11 | 6 | 17 |
| IRONWOOD ESTATES PHASE 3 |  |  |  |  |  |
| SINGLE-FAMILY <br> DETACHED HOUSING | ITE Code 210 | 56 units | 34 | 21 | 55 |
| RECREATIONAL COMMUNITY CENTER | ITE Code 495 | 2,500 sq. ft. | 3 | 3 | 6 |
| THE RIDGE PHASE 1 |  |  |  |  |  |
| SINGLE-FAMILY <br> DETACHED HOUSING | ITE Code 210 | 11 units | 7 | 4 | 11 |
| THE RIDGE PHASE 2 |  |  |  |  |  |
| SINGLE-FAMILY <br> DETACHED HOUSING | ITE Code 210 | 221 units | 137 | 81 | 218 |
| Total Proposed Project Trips |  |  | 192 | 115 | 307 |

## TRIP GENERATION FOR SENSITIVITY SCENARIO

The estimated trip generation for the Sensitivity Scenario was obtained from the John Day Innovation Gateway Area Plan ${ }^{6}$. Overall, the build-out of the proposed land use assumed for the Innovation Gateway Area is expected to generate about 197 (90 in, 107 out) p.m. peak hour trips (see Table 8).
${ }^{6}$ John Day Gateway Transportation Impact Analysis. DKS Associates, March 2020.

TABLE 8: TRIP GENERATION FOR SENSITIVIY SCENARIO

| LAND USE | TRIP GENERATION SOURCE | LAND USE SIZE | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | IN | OUT | TOTAL |
| HOTEL | ITE- Hotel land use (ITE Code 310) | 60 rooms | 18 | 18 | 36 |
| CONFERENCE CENTER | Based on space planning practices, auto occupancy rates and arrival and departure patterns | 6,500 square feet | 38 | 25 | 63 |
| OFFICE | ITE- General Office Building (ITE Code 710) | 42,000 square feet | 7 | 41 | 48 |
| PUBLIC WORKS FACILITY | ITE- Small Office Building (ITE Code 712) | 7 employees | 3 | 5 | 8 |
| PARKS AND OPEN SPACES (I.E., PAVILION, LAWN, OPEN SPACE, BEACH, TRAILS, WATER GARDEN, GREENHOUSES) | ITE- Public Park (ITE Code 411) | 90 acres | 15 | 13 | 28 |
| CAMPGROUND | ITE- Campground/ Recreation Vehicle Park (ITE Code 416) | 50 campsites | 9 | 5 | 14 |
| TOTAL PROPOSED PROJECT TRIPS* |  |  | 90 | 107 | 197 |

* Source: John Day Innovation Gateway Area Plan


## TRIP DISTRIBUTION

Trip distribution involves estimating how project generated traffic will leave and arrive at the proposed site. The trip distribution was estimated based on regional population distribution and current traffic patterns. It is estimated that 20 percent of the traffic would originate or end from the west along W. Main Street, 15 percent from the east along W. Main Street, 15 percent from the south along S. Canyon Boulevard and 50 percent from within John Day.

## SECTION 4: FUTURE CONDITIONS

The following section summarizes the peak hour transportation operating conditions for the planning horizon years of 2023 and 2025. Future traffic operating conditions were analyzed at the study intersections to determine if the transportation network can support traffic generated by the proposed project. If intersection mobility standards are not met, then mitigations may be necessary to improve network performance.

## 2023 BACKGROUND CONDITIONS INTERSECTION OPERATIONS

Table 9 shows the future 2023 intersection operations at study intersections, without the proposed projects. As shown, the background traffic growth is expected to have little impact on traffic operations. All study intersections are expected to operate with a v/c ratio of 0.19 or better.

TABLE 9: 2023 BACKGROUND CONDITIONS STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY <br> STANDARD | DELAY | LOS | V/C |
| :---: | :---: | :---: | :---: | :---: |
| W. MAIN STREET / PATTERSON BRIDGE ROAD | W. Main Street:$0.85 \text { V/C; }$ | 13 | A/B | 0.18 |
| W. MAIN STREET / NW 3RD AVENUE |  | 11 | A/B | 0.10 |
| E. MAIN STREET / NE 3RD AVENUE | Minor: <br> Approaches: 0.95 V/C | 11 | A/B | 0.19 |
| E. MAIN STREET / THE RIDGE ACCESS |  | - | - | - |

$\mathrm{v} / \mathrm{c}=$ Volume-to-Capacity Ratio of Worst Movement
Delay = Average Intersection Delay (sec.) of Worst Approach
LOS = Level of Service of Major Street/Minor Street

## 2023 PROJECT CONDITIONS INTERSECTION OPERATIONS

The 2023 project conditions peak hour operations at study intersection are shown in Table 10. As shown, the added traffic associated with the proposed projects (Ironwood Phase 2 and The Ridge Phase 1) is expected to have little impact on traffic operations when compared to the background conditions without the project (see Table 9 earlier in this document). All study intersections are still expected to operate with a v/c ratio of 0.19 or better.

TABLE 10: 2023 PROJECT CONDITIONS STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY STANDARD | DELAY | LOS | V/C |
| :---: | :---: | :---: | :---: | :---: |
| W. MAIN STREET / PATTERSON BRIDGE ROAD |  | 14 | A/B | 0.18 |
| W. MAIN STREET / NW 3RD AVENUE | W. Main Street: $0.85 \text { V/C; }$ | 11 | A/B | 0.10 |
| E. MAIN STREET / NE 3RD AVENUE | Minor: <br> Approaches: 0.95 | 11 | A/B | 0.19 |
| E. MAIN STREET / THE RIDGE ACCESS |  | 12 | A/B | 0.16 |

$\mathrm{v} / \mathrm{c}=$ Volume-to-Capacity Ratio of Worst Movement
Delay $=$ Average Intersection Delay (sec.) of Worst Approach
LOS = Level of Service of Major Street/Minor Street

## 2025 BACKGROUND CONDITIONS INTERSECTION OPERATIONS

Table 11 shows the future 2025 intersection operations at study intersections, without the Phase 2 (The Ridge) and 3 (Ironwood Estates) proposed projects. As shown, the background traffic growth is expected to have little impact on traffic operations. All study intersections are expected to operate with a v/c ratio of 0.20 or better.

TABLE 11: 2025 BACKGROUND CONDITIONS STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY <br> STANDARD | DELAY | LOS | V/C |
| :--- | :---: | :---: | :---: | :---: |
| W. MAIN STREET / <br> PATTERSON BRIDGE ROAD |  | 14 | A/B | 0.19 |
| W. MAIN STREET / NW 3RD <br> AVENUE | W. Main Street: <br> $0.85 ~ V / C ; ~$ | Minor: | 12 | A/B |

v/c = Volume-to-Capacity Ratio of Worst Movement Delay = Average Intersection Delay (sec.) of Worst Approach LOS = Level of Service of Major Street/Minor Street

The 2025 project conditions peak hour operations at study intersection are shown in Table 12. As shown, the added traffic associated with the proposed projects (Ironwood Phase 3 and The Ridge Phase 2) is expected to have little impact on traffic operations when compared to the background conditions without the project (see Table 11 earlier in this document). All study intersections are still expected to operate with a v/c ratio of 0.28 or better.

TABLE 12: 2025 PROJECT CONDITIONS STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY <br> STANDARD | DELAY | LOS | V/C |
| :---: | :---: | :---: | :---: | :---: |
| W. MAIN STREET / PATTERSON BRIDGE ROAD | W. Main Street:$0.85 \text { V/C; }$ | 15 | A/C | 0.22 |
| W. MAIN STREET / NW 3RD AVENUE |  | 12 | A/B | 0.14 |
| E. MAIN STREET / NE 3RD AVENUE | $\begin{gathered} \text { Minor: } \\ \text { Approaches: } 0.95 \\ \text { V/C } \end{gathered}$ | 14 | A/B | 0.28 |
| E. MAIN STREET / THE RIDGE ACCESS |  | 16 | A/C | 0.25 |

$\mathrm{v} / \mathrm{c}=$ Volume-to-Capacity Ratio of Worst Movement
Delay $=$ Average Intersection Delay (sec.) of Worst Approach
LOS = Level of Service of Major Street/Minor Street

## SECTION 5: RECOMMENDATIONS

The proposed project will not have an impact to the study intersection operations based on projected growth. However, a few improvements are recommended to support the proposed project.

## SITE ACCESS

The Ironwood Estates Phase 3 project has one proposed access to Government Entry Road. Although the proposed driveway would be located 150 feet closer than the 300-foot spacing standard, no operational or safety issues are anticipated due to the low number of vehicles using the driveway, and a deviation to the Code will be required. All other proposed site accesses meet minimum access spacing requirements.

## SIGHT DISTANCE

Prior to occupancy, sight distance at the project driveway will need to be verified, documented, and stamped by a registered professional Civil or Traffic Engineer licensed in the State of Oregon.

## PEDESTRIAN / BICYCLE IMPROVEMENTS

The proposed sites will provide streets with a 25 -foot paved width, allowing for two 10 -foot travel lanes for the circulation of vehicle traffic and a 5 -foot width for pedestrians to walk along the shoulder. Bicyclists will share the roadways with motor vehicles along the internal local streets.

The following sections summarize the Innovation Gateway Area sensitivity scenario, including the network improvements, intersection operations and expected benefits.

## NETWORK IMPROVEMENTS

The following sections summarize the proposed network improvements for pedestrian, bicycle and vehicular travel in and around the Innovation Gateway Area that are included in the sensitivity scenario (summarized in Figure 3 earlier in this document).

## PEDESTRIAN CIRCULATION SYSTEM IMPROVEMENTS

Pedestrians approaching and traveling within the project site will be able to safely and efficiently walk between destinations using a proposed system of sidewalks, multi-use paths and trails. As a primary pedestrian thoroughfare, an improved W Main Street section will include a continuous sidewalk on the north side from downtown John Day to Patterson Bridge Road, and from downtown John Day to the proposed Johnson Drive on the south side. No sidewalk is recommended on the south side west of the proposed Johnson Drive due to the lack of adjacent development and topography constraints. A network of walkways and trails is recommended just to the west of Johnson Drive that would connect to recommended sidewalks on W Main Street at the Johnson Drive intersection. In addition, curb ramps are recommended at each intersection crossing along W Main Street to bring them into Americans with Disabilities Act (ADA) compliance.

The proposed $7^{\text {th }}$ Street extension will serve as the primary pedestrian route north of the John Day River. It will provide a continuous pedestrian connection between Patterson Bridge Road and Bridge Street. This street is proposed to include a 5 -foot sidewalk and a multi-use path will parallel the roadway on the south side.

A 5-foot sidewalk is recommended on the east side of Patterson Bridge Road between W Main Street and the proposed Government Entry Road. The proposed Gateway Drive will also provide a local walkway linking the proposed $7^{\text {th }}$ Street with the proposed Government Road extension. This street is proposed to include a 5 -foot sidewalk on the north side. Government Entry Road is also proposed to include a 5-foot shoulder on each side for pedestrian travel from Patterson Bridge Road to Valley View Drive.

The proposed multi-use path on the south side of the proposed $7^{\text {th }}$ Street will provide a primary walkway along the John Day River. This multi-use path will provide for convenient and comfortable travel and recreation between Patterson Bridge Road, the Oregon Pine and Innovation Gateway areas and the proposed Aquatic Center and existing multi-use pathway network within $7^{\text {th }}$ Street Park, east of Bridge Street. In addition, a proposed network of multi-use paths and trails will link the proposed multi-use path along the John Day River with Hill Family City Park, Davis Creek Park and Campground, Oregon Pine and Innovation Gateway areas and Valley View Drive.

An improved Oregon Pine Bridge and a bridge adjacent to Hill Family City Park will provide new pedestrian crossings of the John Day River, in addition to the existing crossings at Patterson Bridge Road and Bridge Street. This network of river crossings will provide shorter block lengths for the pedestrian system, will increase pedestrian access to destinations, and will also provide a recreational loop trail. An additional bridge crossing will also be provided via 3rd Avenue at the east end of the City.

Safe and comfortable pedestrian crossings will be provided where facilities cross streets. This will include curb extensions and marked crosswalks where appropriate. A pedestrian wayfinding system for the site and the entire downtown area should also be developed.

## BICYCLE CIRCULATION SYSTEM IMPROVEMENTS

The proposed 7th Street extension will serve as a local bikeway, serving those traveling from downtown John Day and the neighborhoods to the north and east. Given the relatively slow vehicular speeds along the proposed street, bicyclists will share travel lanes with vehicular traffic. It is recommended to include sharrows to alert drivers to share the street and be designed to allow bicyclists to travel outside of the door zone of parked vehicles.

In addition, cyclists can travel along the proposed multi-use path along the John Day River between the Oregon Pine and Innovation Gateway areas and Bridge Street. A potential link to Hill Family City Park and 7th Street Park will also connect the site with the multi-use path networks in these parks. This multi-use path will provide for convenient and comfortable bicycle travel between the Oregon Pine and Innovation Gateway areas and Bridge Street.

W Main Street will serve as the primary bikeway south of the John Day River. It is recommended to include 6-foot bike lanes between downtown John Day and Patterson Bridge Road. The recommended bike lanes will also enhance the Old West Oregon Scenic Bikeway through the project area.

The proposed Johnson Drive will connect cyclists from the bike facilities on W Main Street to the Oregon Pine and Innovation Gateway areas. Since it will be a local street and expected to have low traffic volumes and slow vehicular speeds, cyclists will share the travel lanes with vehicular traffic.

Government Entry Road is proposed to include a 5-foot shoulder on each side for bike travel from Patterson Bridge Road to Valley View Drive. Sharrows are also recommended on Patterson Bridge Road between W Main Street and the proposed Government Entry Road.

In addition, it is recommended that bike racks and bike storage zones be incorporated in strategic locations along streetscapes and within future development to encourage bicycle use. A bicycle wayfinding system for the site and the entire downtown area should also be developed. This system could also consider routing to mountain biking opportunities, to enhance the city's reputation for the sport.

## VEHICULAR CIRCULATION SYSTEM IMPROVEMENTS

W Main Street provides primary access to the project site south of the John Day River, with two proposed accesses. One access is proposed to be located approximately 1,100 feet east of Patterson Bridge Road, serving the proposed hotel. The primary site access is proposed to be Johnson Drive, which will be located approximately 900 feet east of the proposed hotel driveway. Left-turn lanes are recommended on W Main Street at both proposed access points, and the Johnson Drive approach to W Main Street is recommended to include separate left-turn and rightturn lanes for exiting traffic.

Another key assumption of the proposed vehicular circulation system is the extension of $7^{\text {th }}$ Street to Patterson Bridge Road north of the John Day River. $7^{\text {th }}$ Street's proposed alignment will provide an alternative route to the highway and a means of vehicular site access to areas north of the river. This new street connection will provide circulation between Patterson Bridge Road and Bridge Street and offer drivers from downtown John Day and neighborhoods to the north and east another option to access the site. An extension of $7^{\text {th }}$ Street at the east end of the City will also link to an additional bridge crossing of the river at Holmstrom Road, to connect $7^{\text {th }}$ Street on the north side of the river with NE 3rd Street on the south side.

North-south running cross-streets, including Patterson Bridge Road and Bridge Street, will link the proposed $7^{\text {th }}$ Street and W Main Street. The proposed Government Entry Road and Gateway Drive will connect $7^{\text {th }}$ Street and Patterson Bridge Road with neighborhoods to the north, further enhancing connectivity north of the river.

## SUMMARY OF BENEFITS

The following sections summarize expected benefits of the network improvements included in the sensitivity scenario.

## TRAVEL TIME / DELAY REDUCTION

To ensure the future roadway network can accommodate the expected growth from the proposed Ironwood Estates (Phase 2 and 3) and The Ridge (Phase 1 and 2) developments, in addition to the potential growth from the Innovation Gateway Area, the future volumes and study intersection operations under the 2025 Project Conditions were tested with the assumed full build-out of these areas, both without and with associated transportation network improvements (see the summary of improvements earlier in this document).

As shown in Table 13, the traffic associated with the assumed full build-out of the Innovation Gateway Area site and rerouted traffic associated with the transportation network improvements is expected to improve intersection operations when compared to the scenario without them.

TABLE 13: 2025 SENSITIVITY SCENARIO STUDY INTERSECTION OPERATIONS (PM PEAK)

| INTERSECTION | MOBILITY STANDARD | WITHOUT IMPROVEMENTS |  |  | WITH IMPROVEMENTS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | DELAY | LOS | v/C | DELAY | LOS | v/C |
| W. MAIN STREET / PATTERSON BRIDGE ROAD | W. Main <br> Street: 0.85 <br> V/C; | 19 | A/C | 0.38 | 14 | A/B | 0.24 |
| W. MAIN STREET / NW 3RD AVENUE |  | 13 | A/B | 0.22 | 13 | A/B | 0.18 |
| E. MAIN STREET / NE 3RD AVENUE | Minor: <br> Approaches: $0.95 \mathrm{~V} / \mathrm{C}$ | 14 | A/B | 0.29 | 17 | A/C | 0.26 |
| E. MAIN STREET / <br> THE RIDGE ACCESS |  | 17 | A/C | 0.26 | 17 | A/C | 0.26 |

$\mathrm{v} / \mathrm{c}=$ Volume-to-Capacity Ratio of Worst Movement
Delay $=$ Average Intersection Delay (sec.) of Worst Approach
LOS = Level of Service of Major Street/Minor Street

The improvement to study intersection operations is a result of the street extensions allowing these trips to occur off the highway (i.e., without using Main Street- US 26), including the 7th Street extension from Bridge Street to Patterson Bridge Road. These new streets remove 960 daily trips from W. Main Street, freeing up capacity at several intersections, as reflected in the reduced $\mathrm{v} / \mathrm{c}$ ratios in Table 13. Total vehicle delay for the minor approaches at the four study intersections during the 2025 pm peak hour is expected to decrease by 924 seconds with the proposed street extensions, from 4,479 seconds to 3,555 seconds.

The estimated travel time for vehicles between Bridge Street and Patterson Bridge Road north of the John Day River, after the extension of 7 th Street, is expected to be 3 minutes, down from 5 minutes today. It is estimated that approximately 730 average daily trips will utilize this route upon build out of the Innovation Gateway Area, with these users expected to experience the full 2 minutes ( 0.03 hours) of travel time savings. This is expected to correspond to a travel time savings of $\$ 143,000 /$ year?

[^6]
## SAFETY

A change in potential collision rates may also occur as a result of these projects:

- Proposed center turn lane along a 2-lane segment of W. Main Street (US 26) from the Patterson Bridge Road intersection across the frontage of the Innovation Gateway Area site, allowing turning vehicles to stop outside of the travel lane, and reduce collision potential. The Patterson Bridge Road intersection has experienced 2 Injury C collisions (i.e., Possible Injury) over the previous 5 -years (see Table 4 earlier in this document) with only 50 left-turns per day. With leftturns at this intersection expected to increase over 6 times (to 320 per day) by 2025, it is assumed that 2 injury C collisions will occur each year without a left-turn lane. Using a crash modification factor of $0.797^{8}$, the installation of a two-way left-turn lane will be expected to reduce injuries by 0.406 annually. This corresponds to a monetized value of $\$ 58,000$ annually ${ }^{9}$.
- The proposed pedestrian/bicycle bridge crossing of the John Day River and parallel trail network will eliminate the need for pedestrians and bicyclists to travel along the shoulder of W. Main Street (US 26). Increased pedestrian and bicycle activity will occur around the Innovation Gateway Area and these projects will eliminate the potential collision risk for these users.


## ALTERNATIVE HIGHWAY ROUTE

The proposed $7^{\text {th }}$ Street extension will provide an alternative route to US 26 through the city, from Patterson Bridge Road to the proposed Holmstrom Road bridge crossing of the John Day River, approximately 1.50 miles in length. This route will provide a link to the existing two vehicle accessible bridge crossings of the John Day River, at Patterson Bridge Road and Bridge Street bridge, in addition to the proposed bridge at Holmstrom Road. This provides an adjacent route to the highway should it close for an adverse event.

Assuming an event causes the closure of US 26 between Patterson Bridge Road and NW $3^{\text {rd }}$ Avenue during the entire pm peak hour of an average weekday, approximately 600 vehicles will be delayed (based on 2025 pm peak volumes east of the Patterson Bridge Road intersection). Using the current vehicle classification data of 4 percent trucks and 96 percent personal vehicles, that would result in travel time delays of $\$ 11,049 /$ hour during the pm peak ${ }^{10}$, while the average off-peak period would result in travel time delays of $\$ 9,612 /$ hour $^{11}$.

[^7]
## BRIDGE

The proposed Holmstrom Road bridge will provide a new connection across the John Day River from the $7^{\text {th }}$ Street east extension to NE $3^{\text {rd }}$ Street, while the proposed $7^{\text {th }}$ Street extension will provide residents and businesses north of the John Day River a continuous connection to each bridge. The City's existing two bridges over the John Day River, Patterson Bridge and the Bridge Street Bridge, were recently rated in Fair condition, and since there are no street connections between these bridges, all traffic flow must cross Bridge Street. Should a flooding event or bridge failure occur at the Bridge Street Bridge, residents and businesses north of the John Day River would have to travel approximately 11 minutes roundtrip ( 0.18 hours) out-of-direction to use the Ranch Road bridge crossing of the river. Currently, 394 average daily vehicle trips utilize the Bridge Street Bridge, which would correspond to travel time loses of \$1,269/day ${ }^{12}$.

[^8]
## APPENDIX

CONTENTS

TRAFFIC COUNTS
ODOT CRASH DATA AND ANALYSIS
SYNCHRO HCM REPORTS

720 SW WASHINGTON STREET, SUITE 500, PORTLAND, OR 97205 • 503.243.3500 • DKSASSOCIATES.COM

## TRAFFIC COUNTS




Main St west of Lyons St Date Start: 31-Jan-19 Latitude: 44' 25.1848 North Longitude: 118' 57.6796 West

| EB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 AxI | 5 Axle | >6 AxI | <6 AxI | 6 Axle | >6 AxI | Not |  |
| Time | Bikes | Trailers | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Classed | Total |
| 01/31/19 | 0 | 2 | 3 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 01:00 | 0 | 1 | 0 | 2 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 02:00 | 0 | 0 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 03:00 | 0 | 2 | 5 | 1 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 04:00 | 0 | 6 | 4 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 |
| 05:00 | 1 | 14 | 15 | 0 | 8 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 44 |
| 06:00 | 0 | 41 | 19 | 2 | 10 | 7 | 0 | 4 | 0 | 2 | 0 | 0 | 0 | 7 | 92 |
| 07:00 | 0 | 95 | 35 | 7 | 35 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 7 | 184 |
| 08:00 | 3 | 80 | 55 | 1 | 31 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 17 | 190 |
| 09:00 | 1 | 90 | 55 | 3 | 35 | 7 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 12 | 207 |
| 10:00 | 3 | 81 | 75 | 2 | 34 | 3 | 0 | 7 | 2 | 0 | 1 | 0 | 0 | 24 | 232 |
| 11:00 | 0 | 95 | 82 | 0 | 37 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 27 | 244 |
| 12 PM | 0 | 98 | 69 | 0 | 40 | 1 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 30 | 241 |
| 13:00 | 2 | 93 | 76 | 1 | 56 | 6 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 28 | 267 |
| 14:00 | 1 | 89 | 67 | 1 | 52 | 2 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 18 | 236 |
| 15:00 | 4 | 105 | 70 | 0 | 47 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 29 | 261 |
| 16:00 | 1 | 121 | 80 | 1 | 54 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 32 | 291 |
| 17:00 | 1 | 92 | 55 | 2 | 45 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 17 | 214 |
| 18:00 | 1 | 61 | 35 | 1 | 23 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 9 | 131 |
| 19:00 | 0 | 34 | 16 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 |
| 20:00 | 0 | 15 | 5 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 26 |
| 21:00 | 0 | 17 | 8 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 32 |
| 22:00 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 23:00 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| Total | 18 | 1233 | 832 | 25 | 539 | 46 | 0 | 32 | 13 | 3 | 1 | 0 | 0 | 265 | 3007 |
| Percent | 0.6\% | 41.0\% | 27.7\% | 0.8\% | 17.9\% | 1.5\% | 0.0\% | 1.1\% | 0.4\% | 0.1\% | 0.0\% | 0.0\% | 0.0\% | 8.8\% |  |
| AM Peak | 08:00 | 07:00 | 11:00 | 07:00 | 11:00 | 06:00 |  | 10:00 | 09:00 | 06:00 | 10:00 |  |  | 11:00 |  |
| Vol. | 3 | 95 | 82 | 7 | 37 | 7 |  | 7 | 3 | 2 | 1 |  |  | 27 |  |
| PM Peak | 15:00 | 16:00 | 16:00 | 17:00 | 13:00 | 13:00 |  | 13:00 | 14:00 |  |  |  |  | 16:00 |  |
| Vol. | 4 | 121 | 80 | 2 | 56 | 6 |  | 4 | 2 |  |  |  |  | 32 |  |
| Grand Total | 18 | 1233 | 832 | 25 | 539 | 46 | 0 | 32 | 13 | 3 | 1 | 0 | 0 | 265 | 3007 |
| Percent | 0.6\% | 41.0\% | 27.7\% | 0.8\% | 17.9\% | 1.5\% | 0.0\% | 1.1\% | 0.4\% | 0.1\% | 0.0\% | 0.0\% | 0.0\% | 8.8\% |  |

Main St west of Lyons St Date Start: 31-Jan-19 Latitude: 44' 25.1848 North Longitude: 118' 57.6796 West

| WB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 AxI | 5 Axle | >6 AxI | <6 AxI | 6 Axle | >6 AxI | Not |  |
| Time | Bikes | Trailers | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Classed | Total |
| 01/31/19 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 5 |
| 01:00 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 |
| 02:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 |
| 03:00 | 0 | 2 | 2 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 8 | 16 |
| 04:00 | 0 | 3 | 3 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 34 |
| 05:00 | 0 | 2 | 4 | 7 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 66 | 82 |
| 06:00 | 0 | 3 | 4 | 7 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 84 | 108 |
| 07:00 | 3 | 6 | 7 | 3 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 154 | 183 |
| 08:00 | 1 | 4 | 8 | 10 | 18 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 152 | 194 |
| 09:00 | 3 | 11 | 16 | 6 | 22 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 142 | 203 |
| 10:00 | 9 | 61 | 46 | 1 | 30 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 84 | 235 |
| 11:00 | 5 | 91 | 62 | 1 | 39 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 53 | 259 |
| 12 PM | 4 | 114 | 70 | 0 | 68 | 3 | 0 | 1 | 2 | 3 | 0 | 0 | 1 | 45 | 311 |
| 13:00 | 5 | 99 | 80 | 1 | 46 | 0 | 0 | 3 | 4 | 1 | 0 | 0 | 1 | 50 | 290 |
| 14:00 | 7 | 92 | 63 | 0 | 51 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 1 | 40 | 260 |
| 15:00 | 6 | 95 | 61 | 2 | 45 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 45 | 260 |
| 16:00 | 4 | 98 | 63 | 1 | 49 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 55 | 276 |
| 17:00 | 3 | 65 | 30 | 0 | 43 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 95 | 237 |
| 18:00 | 0 | 7 | 8 | 1 | 14 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 93 | 125 |
| 19:00 | 2 | 5 | 4 | 1 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 59 | 75 |
| 20:00 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 43 | 50 |
| 21:00 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 31 |
| 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 16 |
| 23:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 7 | 8 |
| Total | 52 | 765 | 535 | 44 | 456 | 7 | 0 | 38 | 9 | 6 | 0 | 0 | 3 | 1356 | 3271 |
| Percent | 1.6\% | 23.4\% | 16.4\% | 1.3\% | 13.9\% | 0.2\% | 0.0\% | 1.2\% | 0.3\% | 0.2\% | 0.0\% | 0.0\% | 0.1\% | 41.5\% |  |
| AM Peak | 10:00 | 11:00 | 11:00 | 08:00 | 11:00 | 09:00 |  | 11:00 | 11:00 | 10:00 |  |  |  | 07:00 |  |
| Vol. | 9 | 91 | 62 | 10 | 39 | 2 |  | 7 | 1 | 1 |  |  |  | 154 |  |
| PM Peak | 14:00 | 12:00 | 13:00 | 15:00 | 12:00 | 12:00 |  | 15:00 | 13:00 | 12:00 |  |  | 12:00 | 17:00 |  |
| Vol. | 7 | 114 | 80 | 2 | 68 | 3 |  | 6 | 4 | 3 |  |  | 1 | 95 |  |
| Grand Total | 52 | 765 | 535 | 44 | 456 | 7 | 0 | 38 | 9 | 6 | 0 | 0 | 3 | 1356 | 3271 |
| Percent | 1.6\% | 23.4\% | 16.4\% | 1.3\% | 13.9\% | 0.2\% | 0.0\% | 1.2\% | 0.3\% | 0.2\% | 0.0\% | 0.0\% | 0.1\% | 41.5\% |  |





| Start <br> Time | $\begin{gathered} \text { 12/19/2019 } \\ \text { Thu } \end{gathered}$ | SB | NB | Combined Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 AM |  | 1 | 1 | 2 |  |
| 01:00 |  | 1 | 2 | 3 |  |
| 02:00 |  | 5 | 3 | 8 |  |
| 03:00 |  | 3 | 0 | 3 |  |
| 04:00 |  | 2 | 1 | 3 |  |
| 05:00 |  | 9 | 20 | 29 |  |
| 06:00 |  | 10 | 46 | 56 |  |
| 07:00 |  | 21 | 52 | 73 |  |
| 08:00 |  | 32 | 32 | 64 |  |
| 09:00 |  | 21 | 35 | 56 |  |
| 10:00 |  | 7 | 15 | 22 |  |
| 11:00 |  | * | * | * |  |
| 12:00 PM |  | * | * | * |  |
| 01:00 |  | * | * | * |  |
| 02:00 |  | * | * | * |  |
| 03:00 |  | * | * | * |  |
| 04:00 |  | * | * | * |  |
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| 08:00 |  | * | * | * |  |
| 09:00 |  | * | * | * |  |
| 10:00 |  | * | * | * |  |
| 11:00 |  | * | * | * |  |
| Total |  | 112 | 207 | 319 |  |
| Percent |  | 35.1\% | 64.9\% |  |  |
| Grand Total |  | 677 | 716 |  |  |
| Percentage |  | 48.6\% | 51.4\% |  |  |
| ADT |  | ADT 892 |  | AADT 892 |  |


| SB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/17/19 | * | * | * | * | * | * | * | * | , | * | * | * | * | * | * | * | * |
| 01:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 02:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 03:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 04:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 05:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 06:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 07:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 08:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 09:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 12 PM | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 13:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 14:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 15:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 16:00 | 34 | 12 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | 22 | 23 |
| 17:00 | 27 | 7 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 21 | 24 |
| 18:00 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 17 | 19 |
| 19:00 | 12 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 19 | 21 |
| 20:00 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 21 | 21 |
| 21:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| 22:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| 23:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| Total | 80 | 25 | 10 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 119 |  |  |
| Percent | 67.2\% | 21.0\% | 8.4\% | 2.5\% | 0.8\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak Vol. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | 16:00 | 16:00 | 16:00 | 16:00 | 17:00 |  |  |  |  |  |  |  |  |  | 16:00 |  |  |
| Vol. | 34 | 12 | 7 | 2 | 1 |  |  |  |  |  |  |  |  |  | 55 |  |  |


| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/18/19 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 01:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 02:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23 | 23 |
| 03:00 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 17 | 19 |
| 04:00 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 19 | 21 |
| 05:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 21 |
| 06:00 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 19 | 23 |
| 07:00 | 15 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 22 | 23 |
| 08:00 | 17 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 21 | 22 |
| 09:00 | 19 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 22 | 23 |
| 10:00 | 23 | 8 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 21 | 23 |
| 11:00 | 32 | 9 | 8 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 22 | 23 |
| 12 PM | 20 | 12 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 22 | 23 |
| 13:00 | 21 | 10 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 21 | 23 |
| 14:00 | 27 | 6 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 20 | 22 |
| 15:00 | 37 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 20 | 23 |
| 16:00 | 45 | 15 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 66 | 21 | 23 |
| 17:00 | 23 | 5 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 22 | 24 |
| 18:00 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22 | 23 |
| 19:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 23 | 23 |
| 20:00 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 21 |
| 21:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 22:00 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 21 |
| 23:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| Total | 305 | 84 | 48 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 446 |  |  |
| Percent | 68.4\% | 18.8\% | 10.8\% | 1.6\% | 0.4\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 11:00 | $11: 00$ | 11:00 | $10: 00$ | 11:00 |  |  |  |  |  |  |  |  |  | 11:00 |  |  |
| Vol. | 32 | 9 | 8 | 1 | 1 |  |  |  |  |  |  |  |  |  | 51 |  |  |
| PM Peak | 16:00 | 16:00 | 12:00 | 17:00 | 16:00 |  |  |  |  |  |  |  |  |  | 16:00 |  |  |
| Vol. | 45 | 15 | 5 | 2 | 1 |  |  |  |  |  |  |  |  |  | 66 |  |  |



| NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/17/19 | * | * | * | * | * | * | * | * | , | * | * | * | * | * | * | * | * |
| 01:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 02:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 03:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 04:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 05:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 06:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 07:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 08:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 09:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 12 PM | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 13:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 14:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 15:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 16:00 | 13 | 5 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 23 | 25 |
| 17:00 | 11 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 21 | 24 |
| 18:00 | 6 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 22 | 23 |
| 19:00 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 17 | 19 |
| 20:00 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 25 | 25 |
| 21:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 23:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| Total | 36 | 10 | 7 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 |  |  |
| Percent | 63.2\% | 17.5\% | 12.3\% | 5.3\% | 1.8\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | 16:00 | 16:00 | 16:00 | 16:00 | 16:00 |  |  |  |  |  |  |  |  |  | 16:00 |  |  |
| Vol. | 13 | 5 | 3 | 1 | 1 |  |  |  |  |  |  |  |  |  | 23 |  |  |


| NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/18/19 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| 01:00 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23 | 23 |
| 02:00 | 3 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 28 | 29 |
| 03:00 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 17 | 19 |
| 04:00 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 25 | 25 |
| 05:00 | 6 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 21 | 24 |
| 06:00 | 31 | 9 | 9 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 23 | 24 |
| 07:00 | 24 | 12 | 5 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 22 | 26 |
| 08:00 | 13 | 7 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 23 | 25 |
| 09:00 | 18 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 21 | 21 |
| 10:00 | 22 | 8 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 21 | 22 |
| 11:00 | 23 | 8 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 21 | 24 |
| 12 PM | 21 | 13 | 8 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 47 | 23 | 25 |
| 13:00 | 29 | 9 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 21 | 23 |
| 14:00 | 20 | 4 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 21 | 24 |
| 15:00 | 24 | 5 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 21 | 24 |
| 16:00 | 27 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 21 | 25 |
| 17:00 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 20 | 21 |
| 18:00 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 20 | 21 |
| 19:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 20:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 27 | 27 |
| 21:00 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 23 | 23 |
| 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | * |
| 23:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| Total | 280 | 95 | 45 | 22 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 452 |  |  |
| Percent | 61.9\% | 21.0\% | 10.0\% | 4.9\% | 1.8\% | 0.4\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 06:00 | 07:00 | 06:00 | 06:00 | 07:00 | 02:00 |  |  |  |  |  |  |  |  | 06:00 |  |  |
| Vol. | 31 | 12 | 9 | 3 | 2 | 1 |  |  |  |  |  |  |  |  | 53 |  |  |
| PM Peak | 13:00 | 12:00 | 12:00 | 12:00 | 15:00 |  |  |  |  |  |  |  |  |  | 12:00 |  |  |
| Vol. | 29 | 13 | 8 | 5 | 1 |  |  |  |  |  |  |  |  |  | 47 |  |  |




| Start Time | $\begin{gathered} \text { 12/18/2019 } \\ \text { Wed } \end{gathered}$ | NB | SB | Combined Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 AM |  | 1 | 2 | 3 | - |
| 01:00 |  | 1 | 0 | 1 | \| |
| 02:00 |  | 0 | 0 | 0 |  |
| 03:00 |  | 1 | 0 | 1 | I |
| 04:00 |  | 3 | 2 | 5 |  |
| 05:00 |  | 1 | 3 | 4 |  |
| 06:00 |  | 8 | 14 | 22 |  |
| 07:00 |  | 7 | 28 | 35 |  |
| 08:00 |  | 13 | 57 | 70 |  |
| 09:00 |  | 21 | 31 | 52 |  |
| 10:00 |  | 38 | 35 | 73 |  |
| 11:00 |  | 35 | 41 | 76 |  |
| 12:00 PM |  | 48 | 42 | 90 |  |
| 01:00 |  | 60 | 54 | 114 |  |
| 02:00 |  | 55 | 50 | 105 |  |
| 03:00 |  | 43 | 60 | 103 |  |
| 04:00 |  | 62 | 61 | 123 |  |
| 05:00 |  | 51 | 41 | 92 |  |
| 06:00 |  | 70 | 43 | 113 |  |
| 07:00 |  | 25 | 38 | 63 |  |
| 08:00 |  | 34 | 18 | 52 |  |
| 09:00 |  | 22 | 18 | 40 |  |
| 10:00 |  | 10 | 8 | 18 |  |
| 11:00 |  | 6 | 5 | 11 |  |
| Total |  | 615 | 651 | 1266 |  |
| Percent |  | 48.6\% | 51.4\% |  |  |


| Start Time | $\begin{gathered} \text { 12/19/2019 } \\ \text { Thu } \end{gathered}$ | NB | SB | Combined Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 AM |  | 1 | 1 | 2 | - |
| 01:00 |  | 1 | 0 | 1 |  |
| 02:00 |  | 1 | 0 | 1 | I |
| 03:00 |  | 1 | 3 | 4 |  |
| 04:00 |  | 1 | 0 | 1 |  |
| 05:00 |  | 1 | 1 | 2 |  |
| 06:00 |  | 10 | 17 | 27 |  |
| 07:00 |  | 5 | 24 | 29 |  |
| 08:00 |  | 20 | 69 | 89 |  |
| 09:00 |  | 34 | 39 | 73 |  |
| 10:00 |  | 30 | 50 | 80 |  |
| 11:00 |  | 21 | 20 | 41 |  |
| 12:00 PM |  | * | * | * |  |
| 01:00 |  | * | * | * |  |
| 02:00 |  | * | * | * |  |
| 03:00 |  | * | * | * |  |
| 04:00 |  | * | * | * |  |
| 05:00 |  | * | * | * |  |
| 06:00 |  | * | * | * |  |
| 07:00 |  | * | * | * |  |
| 08:00 |  | * | * | * |  |
| 09:00 |  | * | * | * |  |
| 10:00 |  | * | * | * |  |
| 11:00 |  | * | * | * |  |
| Total |  | 126 | 224 | 350 |  |
| Percent |  | 36.0\% | 64.0\% |  |  |
| Grand Total |  | 956 | 1054 |  |  |
| Percentage |  | 47.6\% | 52.4\% |  |  |
| ADT |  | ADT 1,272 |  | AADT 1,272 |  |

NW Bridge St south of 7th Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West

| NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/17/19 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 01:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 02:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 03:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 04:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 05:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 06:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 07:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 08:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 09:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 12 PM | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 13:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 14:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 15:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 16:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 17:00 | 40 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 20 | 21 |
| 18:00 | 43 | 14 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 63 | 21 | 23 |
| 19:00 | 19 | 11 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 22 | 24 |
| 20:00 | 22 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 20 | 23 |
| 21:00 | 15 | 7 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 21 | 23 |
| 22:00 | 8 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 22 | 23 |
| 23:00 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 21 |
| Total | 148 | 45 | 16 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 215 |  |  |
| Percent | 68.8\% | 20.9\% | 7.4\% | 2.3\% | 0.0\% | 0.5\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak Vol. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | 18:00 | 18:00 | 19:00 | 19:00 |  | 18:00 |  |  |  |  |  |  |  |  | 18:00 |  |  |
| Vol. | 43 | 14 | 6 | 2 |  | 1 |  |  |  |  |  |  |  |  | 63 |  |  |

NW Bridge St south of 7th
Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West

| NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/18/19 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| 01:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 23 | 23 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 03:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 27 | 27 |
| 04:00 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23 | 23 |
| 05:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 06:00 | 5 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 22 | 23 |
| 07:00 | 3 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 21 | 23 |
| 08:00 | 11 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 20 | 24 |
| 09:00 | 20 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 17 | 19 |
| 10:00 | 18 | 11 | 5 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 23 | 26 |
| 11:00 | 24 | 6 | 1 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 21 | 25 |
| 12 PM | 21 | 14 | 8 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 23 | 25 |
| 13:00 | 21 | 21 | 11 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 23 | 25 |
| 14:00 | 32 | 9 | 10 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | 23 | 24 |
| 15:00 | 26 | 10 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 22 | 23 |
| 16:00 | 43 | 11 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 62 | 21 | 23 |
| 17:00 | 37 | 12 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 21 | 21 |
| 18:00 | 45 | 14 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 22 | 23 |
| 19:00 | 20 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 20 | 21 |
| 20:00 | 21 | 5 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 22 | 23 |
| 21:00 | 18 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 20 | 22 |
| 22:00 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 18 | 21 |
| 23:00 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 21 | 21 |
| Total | 381 | 128 | 71 | 26 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 615 |  |  |
| Percent | 62.0\% | 20.8\% | 11.5\% | 4.2\% | 1.1\% | 0.3\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 11:00 | 10:00 | 10:00 | 11:00 | 03:00 | 10:00 |  |  |  |  |  |  |  |  | 10:00 |  |  |
| Vol. | 24 | 11 | 5 | 3 | 1 | 1 |  |  |  |  |  |  |  |  | 38 |  |  |
| PM Peak | 18:00 | 13:00 | 13:00 | 13:00 | 12:00 |  |  |  |  |  |  |  |  |  | 18:00 |  |  |
| Vol. | 45 | 21 | 11 | 5 | 2 |  |  |  |  |  |  |  |  |  | 70 |  |  |

NW Bridge St south of 7th
Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West

| NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/19/19 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 01:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 02:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 23 | 23 |
| 03:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 04:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 19 |
| 05:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 21 | 21 |
| 06:00 | 8 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 23 | 27 |
| 07:00 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 21 | 21 |
| 08:00 | 15 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 21 | 25 |
| 09:00 | 20 | 9 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 21 | 24 |
| 10:00 | 20 | 5 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 22 | 23 |
| 11:00 | 16 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 21 | 22 |
| 12 PM | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 13:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 14:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 15:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 16:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 17:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 18:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 19:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 20:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 21:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 22:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 23:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| Total | 86 | 23 | 11 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 126 |  |  |
| Percent | 68.3\% | 18.3\% | 8.7\% | 2.4\% | 1.6\% | 0.8\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 09:00 | 09:00 | 10:00 | 08:00 | 06:00 | 10:00 |  |  |  |  |  |  |  |  | 09:00 |  |  |
| Vol. | 20 | 9 | 4 | 2 | 1 | 1 |  |  |  |  |  |  |  |  | 34 |  |  |

PM Peak


Statistics
10 MPH Pace Speed: $15-24$ MPH
Percent in Pace

15 MPH

NW Bridge St south of 7th Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West

| SB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/17/19 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 01:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 02:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 03:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 04:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 05:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 06:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 07:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 08:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 09:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 12 PM | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 13:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 14:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 15:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 16:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
| 17:00 | 32 | 9 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 21 | 21 |
| 18:00 | 40 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 20 | 22 |
| 19:00 | 25 | 4 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 21 | 24 |
| 20:00 | 15 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 18 | 20 |
| 21:00 | 17 | 3 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 22 | 23 |
| 22:00 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 24 | 25 |
| 23:00 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 21 | 21 |
| Total | 134 | 26 | 14 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 179 |  |  |
| Percent | 74.9\% | 14.5\% | 7.8\% | 1.7\% | 0.6\% | 0.6\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak Vol. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | 18:00 | 17:00 | 21:00 | 19:00 | 17:00 | 19:00 |  |  |  |  |  |  |  |  | 18:00 |  |  |
| Vol. | 40 | 9 | 5 | 1 | 1 | 1 |  |  |  |  |  |  |  |  | 50 |  |  |

NW Bridge St south of 7th
Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West

| SB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1 | 21 | 23 | 25 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |  | 85th | 95th |
| Time | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 999 | Total | Percent | Percent |
| 12/18/19 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 21 |
| 01:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | * | * |
| 04:00 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 23 | 23 |
| 05:00 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23 | 23 |
| 06:00 | 9 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 21 | 23 |
| 07:00 | 18 | 7 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 21 | 23 |
| 08:00 | 45 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 21 | 23 |
| 09:00 | 29 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 18 | 20 |
| 10:00 | 22 | 10 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 21 | 23 |
| 11:00 | 28 | 9 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 21 | 23 |
| 12 PM | 24 | 13 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 21 | 23 |
| 13:00 | 31 | 13 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 54 | 22 | 23 |
| 14:00 | 36 | 8 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 21 | 23 |
| 15:00 | 47 | 12 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 20 | 21 |
| 16:00 | 50 | 8 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 61 | 20 | 21 |
| 17:00 | 28 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 21 | 21 |
| 18:00 | 30 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 21 | 21 |
| 19:00 | 29 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 21 | 22 |
| 20:00 | 13 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 22 | 24 |
| 21:00 | 14 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 21 | 23 |
| 22:00 | 5 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 21 | 23 |
| 23:00 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 30 | 31 |
| Total | 464 | 127 | 49 | 9 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 651 |  |  |
| Percent | 71.3\% | 19.5\% | 7.5\% | 1.4\% | 0.2\% | 0.0\% | 0.2\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 08:00 | 10:00 | 08:00 | $11: 00$ | 10:00 |  |  |  |  |  |  |  |  |  | 08:00 |  |  |
| Vol. | 45 | 10 | 6 | 2 | 1 |  |  |  |  |  |  |  |  |  | 57 |  |  |
| PM Peak | 16:00 | 12:00 | 13:00 | 12:00 |  |  | 23:00 |  |  |  |  |  |  |  | 16:00 |  |  |
| Vol. | 50 | 13 | 10 | 2 |  |  | 1 |  |  |  |  |  |  |  | 61 |  |  |

NW Bridge St south of 7th
Date Start: 17-Dec-19 Latitude: 44' 25.3402 North Longitude: 118' 57.2681 West


## ODOT CRASH DATA AND ANALYSIS

| General \& Site Information |  |
| :--- | :--- |
| Analyst: | DKS |
| Agency/Company: |  |
| Date: | $4 / 27 / 2021$ |
| Project Name: | John Day |


| Intersection Crash Data |  |  |  |  |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Intersection | Year |  |  |  |  |  |  |
| Intersection | Type | 2014 | 2015 | 2016 | 2017 | 2018 | Total |  |
| W Main St./ Patterson Brid | Urban 3ST | 0 | 0 | 0 | 1 | 1 | 2 | 1 |
| W Main St./NW 3rd Ave. | Urban 3ST | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| E Main St./NE 3rd Ave. | Urban 3ST | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
|  |  |  |  |  |  |  | 0 | 4 |
|  |  |  |  |  |  |  | 0 | 5 |
|  |  |  |  |  |  |  | 0 | 6 |
|  |  |  |  |  |  |  | 0 | 7 |
|  |  |  |  |  |  |  | 0 | 8 |
|  |  |  |  |  |  |  | 0 | 9 |
|  |  |  |  |  |  |  | 0 | 10 |
|  |  |  |  |  |  |  | 0 | 11 |
|  |  |  |  |  |  |  | 0 | 12 |
|  |  |  |  |  |  |  | 0 | 13 |
|  |  |  |  |  |  |  | 0 | 14 |
|  |  |  |  |  |  |  | 0 | 15 |
|  |  |  |  |  |  |  | 0 | 16 |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  |  |  |  |  |  |  | 0 |  |
|  | Total | 0 | 0 | 0 | 2 | 1 | 3 |  |


| Intersection Population Type Crash Rate |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Average Crash Rate per intersection type |  |  |  |  |  |
| Intersection Pop. Type | Sum of <br> Crashes | Avg Crash <br> sum of 5- <br> yat MEV | Rate for Ref <br> Pop. | INT in Pop |  |
| Rural 3SG | 0 | 0 |  |  |  |
| Rural 3ST | 0 | 0 |  |  |  |
| Rural 4SG | 0 | 0 |  |  |  |
| Rural 4ST | 0 | 0 |  |  |  |
| Urban 3ST | 3 | 21 | 0.1455 | 3 |  |
| Urban 3SG | 0 | 0 |  |  |  |
| Urban 4ST | 0 | 0 |  |  |  |
| Urban 4SG | 0 | 0 |  |  |  |


| Critical Rate Calculation |  |  |  |  |  |  |  |  | APM Exhibit 4-1Mean CrashRate | $\begin{gathered} \begin{array}{c} \text { Statewide } \\ \text { Critical Rate } \end{array} \\ \hline \end{gathered}$ | OverStatewideCritical Critical | APM Exhibit 4-1 90thPercentile Rate | Over 90th |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | AADT Entering Intersection | 5-year MEV | Crash Total | Intersection Population Type | Intersection Crash Rate | Reference <br> Population Crash Rate | Critical <br> Rate | Over Critical |  |  |  |  |  |
| W Main St./ Patterson Brid | 3,900 | 7.1 | 2 | Urban 3ST | 0.281 | APM Exhibit 4-1 |  |  | 0.131 | 0.424 | Under | 0.293 | Under |
| W Main St./NW 3rd Ave. | 4,800 | 8.8 | 0 | Urban 3ST | 0.000 | APM Exhibit 4-1 |  |  | 0.131 | 0.389 | Under | 0.293 | Under |
| E Main St./NE 3rd Ave. | 2,600 | 4.7 | 1 | Urban 3ST | 0.211 | APM Exhibit 4-1 |  |  | 0.131 | 0.510 | Under | 0.293 | Under |

## SYNCHRO HCM REPORTS

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | F |  |  |  |
| Traffic Vol, veh/h | 5 | 195 | 195 | 15 | 45 | 15 |
| Future Vol, veh/h | 5 | 195 | 195 | 15 | 45 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Ven in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 70 | 70 | 70 | 70 | 70 | 70 |
| Heavy Vehicles, \% | 0 | 1 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 7 | 279 | 279 | 21 | 64 | 21 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 300 | 0 | - | 0 | 583 | 290 |
| Stage 1 | - | - | - | - | 290 | - |
| Stage 2 | - | - | - | - | 293 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 1273 | - | - | - | 478 | 754 |
| Stage 1 | - | - | - | - | 764 | - |
| Stage 2 | - | - | - | - | 762 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1273 | - | - | - | 475 | 754 |
| Mov Cap-2 Maneuver | - | - | - | - | 475 | - |
| Stage 1 | - | - | - | - | 759 | - |
| Stage 2 | - | - | - | - | 762 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.2 |  | 0 |  | 13.2 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1273 | - | - | - | 523 |
| HCM Lane V/C Ratio |  | 0.006 | - | - | - | 0.164 |
| HCM Control Delay (s) |  | 7.8 | 0 | - | - | 13.2 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.6 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 25 | 260 | 260 | 25 | 10 | 25 |
| Future Vol, veh/h | 25 | 260 | 260 | 25 | 10 | 25 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 283 | 283 | 27 | 11 | 27 |






| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 307 | 0 | - | 0 | 597 | 297 |
| Stage 1 | - | - | - | - | 297 | - |
| Stage 2 | - | - | - | - | 300 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 1265 | - | - | - | 469 | 747 |
| Stage 1 | - | - | - | - | 758 | - |
| Stage 2 | - | - | - | - | 756 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1265 | - | - | - | 466 | 747 |
| Mov Cap-2 Maneuver | - | - | - | - | 466 | - |
| Stage 1 | - | - | - | - | 753 | - |
| Stage 2 | - | - | - | - | 756 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.2 |  | 0 |  | 13.4 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1265 | - | - | - | 514 |
| HCM Lane V/C Ratio |  | 0.006 | - | - | - | 0.167 |
| HCM Control Delay (s) |  | 7.9 | 0 | - | - | 13.4 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.6 |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 25 | 265 | 265 | 25 | 10 | 25 |
| Future Vol, veh/h | 25 | 265 | 265 | 25 | 10 | 25 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 288 | 288 | 27 | 11 | 27 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 315 | 0 | - | 0 | 644 | 302 |
| Stage 1 | - | - | - | - | 302 | - |
| Stage 2 | - | - | - | - | 342 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1245 | - | - | - | 437 | 738 |
| Stage 1 | - | - | - | - | 750 | - |
| Stage 2 | - | - | - | - | 719 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1245 | - | - | - | 426 | 738 |
| Mov Cap-2 Maneuver | - | - | - | - | 426 | - |
| Stage 1 | - | - | - | - | 731 | - |
| Stage 2 | - | - | - | - | 719 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.7 |  | 0 |  | 11.3 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1245 | - | - | - | 610 |
| HCM Lane V/C Ratio |  | 0.022 | - | - | - | 0.062 |
| HCM Control Delay (s) |  | 8 | 0 | - | - | 11.3 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.2 |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\mathbf{- 1}$ | $\mathbf{T}$ |  | M |  |
| Traffic Vol, veh/h | 5 | 203 | 202 | 15 | 45 | 15 |
| Future Vol, veh/h | 5 | 203 | 202 | 15 | 45 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 70 | 70 | 70 | 70 | 70 | 70 |
| Heavy Vehicles, \% | 0 | 1 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 7 | 290 | 289 | 21 | 64 | 21 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |
| Movement | WBL | WBR | SEL | SET | NWT | NWR |
| Lane Configurations | $\mathbf{r}$ |  | 1 | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 5 | 51 | 62 | 285 | 270 | 10 |
| Future Vol, veh/h | 5 | 51 | 62 | 285 | 270 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 100 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 84 | 84 | 84 | 84 | 84 | 84 |
| Heavy Vehicles, \% | 0 | 0 | 1 | 0 | 3 | 0 |
| Mvmt Flow | 6 | 61 | 74 | 339 | 321 | 12 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 814 | 327 | 333 | 0 | - | 0 |
| Stage 1 | 327 | - | - | - | - | - |
| Stage 2 | 487 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.11 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.209 | - | - | - |
| Pot Cap-1 Maneuver | 350 | 719 | 1232 | - | - | - |
| Stage 1 | 735 | - | - | - | - | - |
| Stage 2 | 622 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 329 | 719 | 1232 | - | - | - |
| Mov Cap-2 Maneuver | 329 | - | - | - | - | - |
| Stage 1 | 691 | - | - | - | - | - |
| Stage 2 | 622 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | SE |  | NW |  |
| HCM Control Delay, s | 11.2 |  | 1.4 |  | 0 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NWT NWRWBLn1 |  |  | SEL | SET |
| Capacity (veh/h) |  | - | - | 650 | 1232 | - |
| HCM Lane V/C Ratio |  | - | - | 0.103 | 0.06 | - |
| HCM Control Delay (s) |  | - | - | 11.2 | 8.1 | - |
| HCM Lane LOS |  | - | - | B | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0.2 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  |  | $\uparrow$ |  | 1 |  |
| Traffic Vol, veh/h | 25 |  | 268 | 25 | 10 | 25 |
| Future Vol, veh/h | 25 | 268 | 268 | 25 | 10 | 25 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 291 | 291 | 27 | 11 | 27 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 318 | 0 | - | 0 | 650 | 305 |
| Stage 1 | - | - | - | - | 305 | - |
| Stage 2 | - | - | - | - | 345 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1242 | - | - | - | 434 | 735 |
| Stage 1 | - | - | - | - | 748 | - |
| Stage 2 | - | - | - | - | 717 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1242 | - | - | - | 423 | 735 |
| Mov Cap-2 Maneuver | - | - | - | - | 423 | - |
| Stage 1 | - | - | - | - | 729 | - |
| Stage 2 | - | - | - | - | 717 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.7 |  | 0 |  | 11.3 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1242 | - | - | - | 607 |
| HCM Lane V/C Ratio |  | 0.022 | - | - | - | 0.063 |
| HCM Control Delay (s) |  | 8 | 0 | - | - | 11.3 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | - | rin |  |
| Traffic Vol, veh/h | 256 | 2 | 0 | 257 | 2 | 0 |
| Future Vol, veh/h | 256 | 2 | 0 | 257 | 2 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 278 | 2 | 0 | 279 | 2 | 0 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 280 | 0 | 558 | 279 |
| Stage 1 | - | - | - | - | 279 | - |
| Stage 2 | - | - | - | - | 279 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1283 | - | 491 | 760 |
| Stage 1 | - | - | - | - | 768 | - |
| Stage 2 | - | - | - | - | 768 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1283 | - | 491 | 760 |
| Mov Cap-2 Maneuver | - | - | - | - | 491 | - |
| Stage 1 | - | - | - | - | 768 | - |
| Stage 2 | - | - | - | - | 768 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 12.4 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | 2 WBL WBT |  |
| Capacity (veh/h) |  | 491 | - | - | 1283 | - |
| HCM Lane V/C Ratio |  | 0.004 | - | - | - | - |
| HCM Control Delay (s) |  | 12.4 | - | - | 0 | - |
| HCM Lane LOS |  | B | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\mathbf{r}$ |  | M |  |
| Traffic Vol, veh/h | 10 | 205 | 205 | 20 | 50 | 20 |
| Future Vol, veh/h | 10 | 205 | 205 | 20 | 50 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 70 | 70 | 70 | 70 | 70 | 70 |
| Heavy Vehicles, \% | 0 | 1 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 14 | 293 | 293 | 29 | 71 | 29 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\mathbf{A}$ | $\uparrow$ |  | 1 |  |
| Traffic Vol, veh/h | 30 | 275 | 275 | 30 | 15 | 30 |
| Future Vol, veh/h | 30 | 275 | 275 | 30 | 15 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 33 | 299 | 299 | 33 | 16 | 33 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 332 | 0 | - | 0 | 681 | 316 |
| Stage 1 | - | - | - | - | 316 | - |
| Stage 2 | - | - | - | - | 365 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1227 | - | - | - | 416 | 724 |
| Stage 1 | - | - | - | - | 739 | - |
| Stage 2 | - | - | - | - | 702 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1227 | - | - | - | 403 | 724 |
| Mov Cap-2 Maneuver | - | - | - | - | 403 | - |
| Stage 1 | - | - | - | - | 715 | - |
| Stage 2 | - | - | - | - | 702 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.8 |  | 0 |  | 11.9 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1227 | - | - | - | 572 |
| HCM Lane V/C Ratio |  | 0.027 | - | - | - | 0.086 |
| HCM Control Delay (s) |  | 8 | 0 | - | - | 11.9 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.3 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | $\uparrow$ | Mr |  |
| Traffic Vol, veh/h | 260 | 5 | 5 | 260 | 5 | 5 |
| Future Vol, veh/h | 260 | 5 | 5 | 260 | 5 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 283 | 5 | 5 | 283 | 5 | 5 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 288 | 0 | 579 | 286 |
| Stage 1 | - | - | - | - | 286 | - |
| Stage 2 | - | - | - | - | 293 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1274 | - | 477 | 753 |
| Stage 1 | - | - | - | - | 763 | - |
| Stage 2 | - | - | - | - | 757 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1274 | - | 475 | 753 |
| Mov Cap-2 Maneuver | - | - | - | - | 475 | - |
| Stage 1 | - | - | - | - | 763 | - |
| Stage 2 | - | - | - | - | 753 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.1 |  | 11.3 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 583 | - | - | 1274 | - |
| HCM Lane V/C Ratio |  | 0.019 | - |  | 0.004 | - |
| HCM Control Delay (s) |  | 11.3 | - | - | 7.8 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 10 | 240 | 226 | 20 | 50 | 20 |
| Future Vol, veh/h | 10 | 240 | 226 | 20 | 50 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 70 | 70 | 70 | 70 | 70 | 70 |
| Heavy Vehicles, \% | 0 | 1 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 14 | 343 | 323 | 29 | 71 | 29 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 352 | 0 | 0 | 0 | 709 | 338 |
| Stage 1 | - |  | - | - | 338 | - |
| Stage 2 | - |  | - | - | 371 | - |
| Critical Hdwy | 4.1 |  | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - |  | - - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - |  | - - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 |  | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 1218 |  | - | - | 404 | 709 |
| Stage 1 | - |  | - - | - | 727 | - |
| Stage 2 | - |  | - - | - | 702 | - |
| Platoon blocked, \% |  |  | - | - |  |  |
| Mov Cap-1 Maneuver | 1218 |  | - - | - | 398 | 709 |
| Mov Cap-2 Maneuver | - |  | - - | - | 398 | - |
| Stage 1 | - |  | - - | - | 717 | - |
| Stage 2 | - |  | - - | - | 702 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.3 |  | 0 |  | 15.1 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL EBT WBT WBR SBLn1 |  |  |  |  |
| Capacity (veh/h) |  | 1218 | - | - | - | 455 |
| HCM Lane V/C Ratio |  | 0.012 | 2 | - | - | 0.22 |
| HCM Control Delay (s) |  | 8 | 80 | - | - | 15.1 |
| HCM Lane LOS |  | A | A A | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | 0 | - | - | 0.8 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | ${ }_{4}$ | $\uparrow$ |  | * |  |
| Traffic Vol, veh/h | 30 | 395 | 349 | 30 | 15 | 30 |
| Future Vol, veh/h | 30 | 395 | 349 | 30 | 15 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 33 | 429 | 379 | 33 | 16 | 33 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 412 | 0 | - | 0 | 891 | 396 |
| Stage 1 | - | - | - | - | 396 | - |
| Stage 2 | - | - | - | - | 495 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1147 | - | - | - | 313 | 653 |
| Stage 1 | - | - | - | - | 680 | - |
| Stage 2 | - | - | - | - | 613 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1147 | - | - | - | 301 | 653 |
| Mov Cap-2 Maneuver | - | - | - | - | 301 | - |
| Stage 1 | - | - | - | - | 654 | - |
| Stage 2 | - | - | - | - | 613 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.6 |  | 0 |  | 13.5 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1147 | - | - | - | 470 |
| HCM Lane V/C Ratio |  | 0.028 | - | - | - | 0.104 |
| HCM Control Delay (s) |  | 8.2 | 0 | - | - | 13.5 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.3 |



| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 419 | 0 | 698 | 353 |
| Stage 1 | - | - | - | - | 353 | - |
| Stage 2 | - | - | - | - | 345 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1140 | - | 407 | 691 |
| Stage 1 | - | - | - | - | 711 | - |
| Stage 2 | - | - | - | - | 717 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1140 | - | 395 | 691 |
| Mov Cap-2 Maneuver | - | - | - | - | 395 | - |
| Stage 1 | - | - | - | - | 711 | - |
| Stage 2 | - | - | - | - | 696 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.7 |  | 15.9 |  |
| HCM LOS |  | C |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mumt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 429 | - | - | 1140 | - |
| HCM Lane V/C Ratio |  | 0.231 | - | - | 0.025 | - |
| HCM Control Delay (s) |  | 15.9 | - | - | 8.2 | 0 |
| HCM Lane LOS |  | C | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.9 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\mathbf{- 1}$ | $\mathbf{T}$ |  | M |  |
| Traffic Vol, veh/h | 11 | 256 | 239 | 26 | 83 | 28 |
| Future Vol, veh/h | 11 | 256 | 239 | 26 | 83 | 28 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 70 | 70 | 70 | 70 | 70 | 70 |
| Heavy Vehicles, \% | 0 | 1 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 16 | 366 | 341 | 37 | 119 | 40 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 378 | 0 | - | 0 | 758 | 360 |
| Stage 1 | - | - | - | - | 360 | - |
| Stage 2 | - | - | - | - | 398 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 1192 | - | - | - | 378 | 689 |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 683 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1192 | - | - | - | 372 | 689 |
| Mov Cap-2 Maneuver | - | - | - | - | 372 | - |
| Stage 1 | - | - | - | - | 698 | - |
| Stage 2 | - | - | - | - | 683 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.3 |  | 0 |  | 18.6 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1192 | - | - | - | 421 |
| HCM Lane V/C Ratio |  | 0.013 | - | - | - | 0.377 |
| HCM Control Delay (s) |  | 8.1 | 0 | - | - | 18.6 |
| HCM Lane LOS |  | A | A | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 1.7 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\mathbf{A}$ | $\mathbf{f}$ |  | 1 |  |
| Traffic Vol, veh/h | 30 | 411 | 363 | 30 | 15 | 30 |
| Future Vol, veh/h | 30 | 411 | 363 | 30 | 15 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 33 | 447 | 395 | 33 | 16 | 33 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 436 | 0 | 729 | 370 |
| Stage 1 | - | - | - | - | 370 | - |
| Stage 2 | - | - | - | - | 359 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1124 | - | 390 | 676 |
| Stage 1 | - | - | - | - | 699 | - |
| Stage 2 | - | - | - | - | 707 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1124 | - | 378 | 676 |
| Mov Cap-2 Maneuver | - | - | - | - | 378 | - |
| Stage 1 | - | - | - | - | 699 | - |
| Stage 2 | - | - | - | - | 686 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.7 |  | 16.5 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mumt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 412 | - | - | 1124 | - |
| HCM Lane V/C Ratio |  | 0.24 | - | - | 0.025 | - |
| HCM Control Delay (s) |  | 16.5 | - | - | 8.3 | O |
| HCM Lane LOS |  | C | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.9 | - | - | 0.1 | - |



| Major/Minor | Major1 |  | Major2 |  | inor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 339 | 0 | - | 0 | 754 | 325 |
| Stage 1 | - | - | - | - | 325 | - |
| Stage 2 | - | - | - | - | 429 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 1231 | - | - | - | 380 | 721 |
| Stage 1 | - | - | - | - | 737 | - |
| Stage 2 | - | - | - | - | 661 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1231 | - | - | - | 366 | 721 |
| Mov Cap-2 Maneuver | - | - | - | - | 366 | - |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 661 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 1 |  | 0 |  | 14.1 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT WBT |  | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1231 | - | - | - | 515 |
| HCM Lane V/C Ratio |  | 0.037 | - | - | - | 0.236 |
| HCM Control Delay (s) |  | 8 | - | - | - | 14.1 |
| HCM Lane LOS |  | A | - | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.9 |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 421 | 0 | - | 0 | 852 | 388 |
| Stage 1 | - | - | - |  | 388 | - |
| Stage 2 | - | - | - | - | 464 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1138 | - | - | - | 330 | 660 |
| Stage 1 | - | - | - |  | 686 | - |
| Stage 2 | - | - | - | - | 633 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1138 | - | - | - | 318 | 660 |
| Mov Cap-2 Maneuver | - | - | - | - | 318 | - |
| Stage 1 | - | - | - |  | 661 | - |
| Stage 2 | - | - | - |  | 633 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.6 |  | 0 |  | 17.1 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mumt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1138 | - | - | - | 389 |
| HCM Lane V/C Ratio |  | 0.029 | - | - | - | 0.238 |
| HCM Control Delay (s) |  | 8.3 | 0 | - | - | 17.1 |
| HCM Lane LOS |  | A | A | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.9 |





[^0]:    ${ }^{1}$ Based on traffic counts conducted during December 2019.

[^1]:    ${ }^{2}$ Table 6, Policy 1F, Oregon Highway Plan, Oregon Department of Transportation, Amended May 2015. ${ }^{3}$ ODOT reported collisions for January 1, 2014 through December 31, 2018.

[^2]:    DKS

[^3]:    *Source: City of John Day Development Code

[^4]:    ${ }^{4}$ John Day Transportation System Plan

[^5]:    ${ }^{5}$ Trip Generation Manual, Institute of Transportation Engineers, $10^{\text {th }}$ Edition.

[^6]:    7 Value of travel time savings $=$ Value of time $\times$ Change in trip time $\times$ Affected trips $=\$ 17.90 /$ hour $\times 0.03$ hours x 730 average daily trips $=\$ 392 /$ day or $\$ 143,000 /$ year. Hourly value of travel of time of $\$ 17.90 /$ hour for All-Purpose trips, based on Revised Departmental Guidance on Valuation of Travel Time in Economic Analysis. Affected trips based on 73 peak hour trips or 730 daily trips.

[^7]:    ${ }^{8}$ CMF ID 2341. Install two-way left-turn lane on a two-lane road. Estimated Annual Injuries Prevented = Current Annual Injury Estimate $\times[1-\mathrm{CMF}]=2 \times[1-0.797]=0.406 /$ year.
    ${ }^{9}$ Safety Benefits $=$ Baseline Risk $\times$ Risk Reduction $\times$ Expected Consequences $=2$ crashes $/$ year $\times 20 \%$ risk reduction $\times[2 \times \$ 72,500]=\$ 58,000 / y e a r$. Risk reduction based on crash reduction factor of 20.3 for CMF ID 2341. Expected consequences based on KABCO Level C - Possible Injury value of $\$ 72,500$.
    ${ }^{10}$ Hourly value of travel of time of $\$ 17.90 /$ hour for All-Purpose personal vehicles trips and $\$ 30.90 /$ hour for truck drivers, based on Revised Departmental Guidance on Valuation of Travel Time in Economic Analysis. Value of travel time savings $=[\$ 17.90 /$ hour $\times 1$ hour $\times 576$ personal vehicles $=\$ 10,310 /$ hour during the pm peak] $+[\$ 30.90 /$ hour $\times 1$ hour $\times 24$ trucks $=\$ 739 /$ hour during the pm peak] $=\$ 11,049 /$ hour during the pm peak.
    ${ }^{11}$ Based on the proportion of the hourly tube count data to peak hour data along US 26 east of Patterson Bridge Road, using the average hourly volume between 8 am and 6 pm of $87 \%$ of peak hour volumes.

[^8]:    ${ }^{12}$ Value of travel time savings $=\$ 17.90 /$ hour $\times 0.18$ hours $\times 394$ average daily trips $=\$ 1,269 /$ day. Hourly value of travel of time of $\$ 17.90$ /hour for All-Purpose trips, based on Revised Departmental Guidance on Valuation of Travel Time in Economic Analysis.

